

Solution for Homework Assignment No. 3

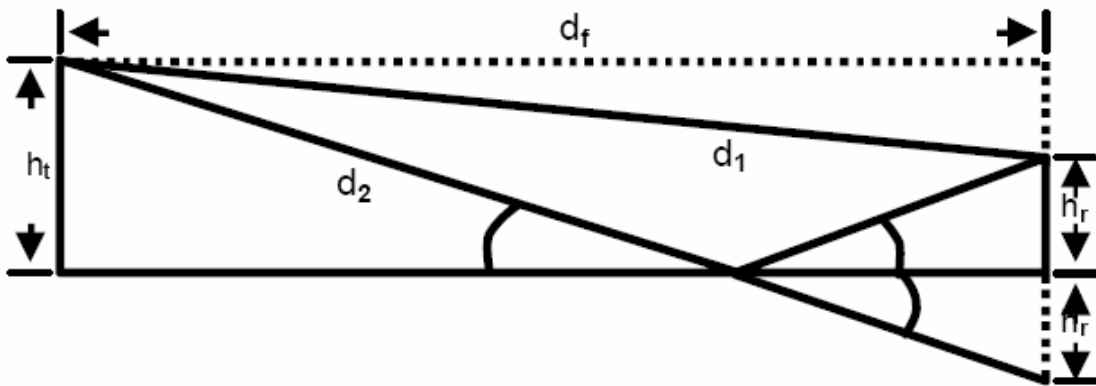
Problem 1 Rappaport, p. 169, Problem 4.15

Let d_f be the physical T-R separation.

d_1 is the free space propagation path length.

d_2 is the ground-reflected path length.

The first Fresnel zone is defined by a d_f that satisfies $d_2 = d_1 + \lambda/2$.



Note that d_2 is drawn using the reflection of h_t to make the calculation easier. Also note that in this drawing $h_t > h_r$, but the same calculation applies for $h_t < h_r$.

$$d_1 = \sqrt{d_f^2 + (h_t - h_r)^2}$$

$$d_2 = \sqrt{d_f^2 + (h_t + h_r)^2}$$

$$\sqrt{d_f^2 + (h_t + h_r)^2} = \sqrt{d_f^2 + (h_t - h_r)^2} + \frac{\lambda}{2}$$

$$d_f^2 + (h_t + h_r)^2 = d_f^2 + (h_t - h_r)^2 + \frac{\lambda^2}{4} + \lambda \sqrt{d_f^2 + (h_t - h_r)^2}$$

$$2h_t h_r = -2h_t h_r + \frac{I^2}{4} + I \sqrt{d_f^2 + (h_t - h_r)^2}$$

$$d_f^2 + (h_t - h_r)^2 = \frac{1}{I^2} \left(4h_t h_r - \frac{I^2}{4} \right)^2$$

$$d_f^2 = \frac{1}{I^2} \left(16h_t^2 h_r^2 - 2h_t h_r I^2 + \frac{I^4}{16} \right) - (h_t^2 - 2h_t h_r + h_r^2)$$

$$d_f^2 = \frac{1}{I^2} \left(16h_t^2 h_r^2 + \frac{I^4}{16} - h_t^2 I^2 - h_r^2 I^2 \right) = \frac{1}{I^2} \left(\frac{I^2}{4} - 4h_t^2 \right) \left(\frac{I^2}{4} - 4h_r^2 \right)$$

$$d_f = \frac{\sqrt{(I^2 - 16h_t^2)(I^2 - 16h_r^2)}}{4I}$$

Had we used the parallel ray approximation, we would have received:

$$S = d_2 - d_1 = \frac{2h_t h_r}{d_f} = \frac{I}{2}$$

$$d_f = \frac{4h_t h_r}{I}$$

Which is correct only if the carrier wavelength is very small in comparison with the receiver and transmitter heights.

Problem 2

Rappaport, p. 170, Problem 4.19

$$P_t = 10\text{w} = 40\text{dBm}$$

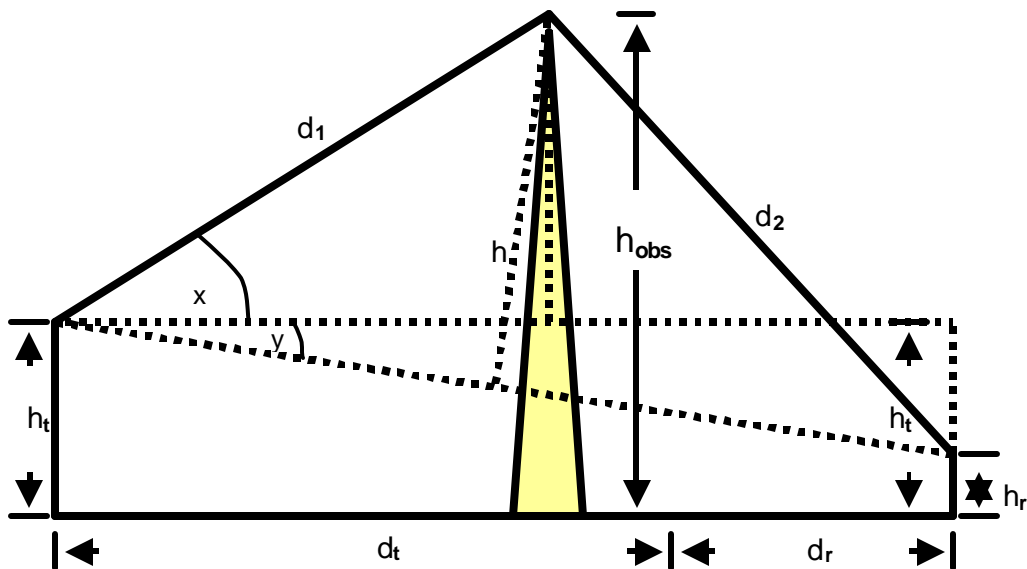
$$G_t = 10\text{dB}$$

$$G_r = 3\text{dB}$$

$$L = 1\text{dB} @ 900\text{MHz}$$

$$f = 900\text{MHz}$$

$$\therefore \lambda = \frac{c}{f} = \frac{1}{3}\text{m}$$



$$h_t = 60\text{m}$$

$$d_t = 3000\text{m}$$

$$h_r = 5\text{m}$$

$$d_r = 2000\text{m}$$

$$h_{obs} = 400\text{m}$$

First, let's compute the free-space model:

$$PL = \frac{I^2}{[4p(d_t + d_r)]^2} = 2.81 \cdot 10^{-11} = -105.5 \text{ dB}$$

$$P_{rec, dBm} = P_{tr, dBm} + PL + G_{t, dB} + G_{r, dB} - L_{dB} = 40 - 105.5 + 10 + 3 - 1 = -53.5 \text{ dBm} = 4.47 \cdot 10^{-9} \text{ W}$$

We should extract h from the geometry of the problem

$$d_1 = \sqrt{d_t^2 + (h_{obs} - h_t)^2} = 3019 \text{ m}$$

$$x = \arctan\left(\frac{h_{obs} - h_t}{d_t}\right) = 6.47^\circ$$

$$y = \arctan\left(\frac{h_t - h_r}{d_t + d_r}\right) = 0.63^\circ$$

$$h = d_1 \cdot \sin(x + y) = 373.15 \text{ m}$$

$$v = h \cdot \sqrt{2 \left(\frac{1}{d_1} + \frac{1}{d_2} \right)} = 26.39$$

$$G_{d, dB} = 20 \log\left(\frac{0.225}{v}\right) = -41.39 \text{ dB}$$

And then, the received power is:

$$P_{rec} = P_{tr, dBm} + PL + G_{t, dB} + G_{r, dB} - L_{dB} + G_{d, dB} = -94.89 \text{ dBm} = 3.24 \cdot 10^{-13} \text{ W}$$

The received power is $3.24 \cdot 10^{-13}$ watts.

Without the obstacle, it would have been $4.47 \cdot 10^{-9}$ watts.

The path loss caused by diffraction is 41.39 dB .

Problem 3

Rappaport, p. 170, Problem 4.20

(a)

$$f = 50 \text{ Mhz}$$

$$\therefore \lambda = c/f = 6 \text{ m}$$

$$PL = \frac{I^2}{[4p(d_t + d_r)]^2} = 9.12 \cdot 10^{-9} = -80.4 \text{ dB}$$

Without diffraction:

$$P_{rec,dBm} = P_{tr,dBm} + PL + G_{t,dB} + G_{r,dB} - L_{dB} = -28.4 \text{ dBm} = 1.45 \cdot 10^{-6} \text{ w}$$

And with diffraction:

$$v = h \cdot \sqrt{\frac{2}{\lambda} \left(\frac{1}{d_1} + \frac{1}{d_2} \right)} = 6.22$$

$$G_{d,dB} = 20 \log \left(\frac{0.225}{v} \right) = -28.83 \text{ dB}$$

$$P_{rec,dBm} = P_{tr,dBm} + PL + G_{t,dB} + G_{r,dB} - L_{dB} + G_{d,dB} = -57.23 \text{ dBm} = 1.89 \cdot 10^{-9} \text{ w}$$

The received power is $1.89 \cdot 10^{-9}$ watts.

Without the obstacle, it would have been $1.45 \cdot 10^{-6}$ watts.

The path loss caused by diffraction is 28.83 dB.

(b)

$$f = 1900 \text{ Mhz}$$

$$\therefore \lambda = c/f = 0.158 \text{ m}$$

$$PL = \frac{I^2}{[4p(d_t + d_r)]^2} = 6.24 \cdot 10^{-12} = -112.05 \text{ dB}$$

Without diffraction:

$$P_{rec,dBm} = P_{tr,dBm} + PL + G_{t,dB} + G_{r,dB} - L_{dB} = -60.05 \text{ dBm} = 9.89 \cdot 10^{-10} \text{ w}$$

And with diffraction:

$$v = h \cdot \sqrt{2 \left(\frac{1}{d_1} + \frac{1}{d_2} \right)} = 38.32$$

$$G_{d,dB} = 20 \log \left(\frac{0.225}{v} \right) = -44.62 \text{ dB}$$

$$P_{rec,dBm} = P_{tr,dBm} + PL + G_{t,dB} + G_{r,dB} - L_{dB} + G_{d,dB} = -104.67 \text{ dBm} = 3.41 \cdot 10^{-14} \text{ W}$$

The received power is $3.41 \cdot 10^{-14}$ watts.

Without the obstacle, it would have been $9.89 \cdot 10^{-10}$ watts.

The path loss caused by diffraction is 44.62 dB .

Problem 4

Rappaport, p. 170, Problem 4.22

$$P_0 = 1 \text{ mW} = 0 \text{ dBm}$$

$$d_0 = 1 \text{ m}$$

$$d = 10 \text{ m}$$

$$\bar{n} = 3.5$$

We require 10% of the measurements to be stronger than -25 dBm .

$$\text{i.e. } \Pr\{P_{rec} > -25 \text{ dBm}\} = 0.9$$

We should first find the mean path loss and then look it up in the Q-function table.

$$\overline{P_{rec}} = P_0 - 10 \cdot \bar{n} \cdot \log \left(\frac{d}{d_0} \right) = -35 \text{ dB}$$

$$Q \left(\frac{X - m}{s} \right) = Q \left(\frac{(-35) - (-25)}{s} \right) = Q \left(\frac{-10}{s} \right) = 0.9$$

$$Q \left(\frac{10}{s} \right) = 0.1 \rightarrow \frac{10}{s} = 1.28$$

$$s = 7.81 \text{ dB}$$

The standard deviation would be 7.81 dB

Problem 5

Rappaport, p. 172, Problem 4.27

$$P_{tr} = 15\text{w} = 41.76\text{dBm}$$

$$G_t = 12\text{dB} = 15.84$$

$$G_r = 3\text{dB} = 2$$

$$BW_r = 30\text{kHz}$$

$$F_{rec} = 8\text{dB}$$

$$f_c = 1800\text{MHz}$$

$$\therefore \mathbf{l} = 0.167\text{m}$$

$$n = 4$$

$$\mathbf{s} = 8\text{dB}$$

$$d_0 = 1000\text{m}$$

We require 20 dB SNR 95% percent of the time

$$\text{i.e. } \Pr\{\text{SNR} > 20\text{dB}\} = 0.95$$

What is the maximum T-R separation that will ensure that SNR?

We first compute the noise threshold, and then the required received power.

Thermal noise spectral density at room temperature:

$$KT = -204\text{dB} \frac{\text{w}}{\text{Hz}} = 3.98 \cdot 10^{-21} \frac{\text{w}}{\text{Hz}}$$

So the thermal noise at the receives is

$$KT \cdot BW_r = 1.194 \cdot 10^{-16} = -129.2\text{dBm}$$

And the noise floor is:

$$F_{rec} + KT \cdot BW_r = -121.2\text{dBm}$$

Regarding the SNR:

$$\Pr\{\text{SNR} > 20\text{dB}\} = Q\left(\frac{20 - \overline{\text{SNR}}}{8}\right) = 0.95$$

$$Q\left(\frac{\overline{\text{SNR}} - 20}{8}\right) = 1 - 0.95 = 0.05$$

$$\frac{\overline{\text{SNR}} - 20}{8} = 1.645$$

$$\overline{\text{SNR}} = 33.16\text{dB}$$

The required received power will be:

$$P_{rec, \min} = -121.2 + 33.16 = -88.04 \text{ dBm}$$

The Power at d_0 :

$$P_0 = \frac{P_{tr} G_t G_r I^2}{(4\pi d_0)^2} = 8.39 \cdot 10^{-8} \text{ W} = -40.76 \text{ dBm}$$

$$P_{rec, \min} = P_0 - 10n \cdot \log\left(\frac{d_{\max}}{d_0}\right)$$

$$\therefore d_{\max} = d_0 \cdot 10^{\frac{P_{0, \text{dBm}} - P_{rec, \min}}{10n}} = 15.2 \text{ km}$$

Problem 6

Rappaport, p. 172, Problem 4.28

$$SNR_{req} = 25dB$$

$$f_c = 900MHz$$

$$\therefore I = 0.333m$$

$$EIRP = P_{tr}G_t = 100W = 50dBm$$

$$G_r = 0dB = 1$$

$$AMPS \rightarrow BW = 30KHz$$

$$F = 10dB$$

$$d = 10km$$

$$\bar{n} = 4$$

$$s = 8dB$$

$$d_0 = 1km$$

We will find P_0 , and then the average received power.

$$P_0 = \frac{P_{tr}G_tG_rI^2}{(4\pi d_0)^2} = \frac{EIRP \cdot G_r I^2}{(4\pi d_0)^2} = 7.02 \cdot 10^{-8}W = -41.54dBm$$

$$\overline{P_{rec}} = P_0 - 10\bar{n} \cdot \log\left(\frac{d}{d_0}\right) = -81.54dBm$$

The thermal noise, just like in problem 4.27, is:

$$KT \cdot BW_r = 1.194 \cdot 10^{-16} = -129.2dBm$$

And the noise floor

$$NF = F_{rec} + KT \cdot BW_r = -119.2dBm$$

The mean SNR:

$$\overline{SNR} = \overline{P_{rec}} - NF = 37.66dB$$

$$\Pr\{SNR > 25dB\} = Q\left(\frac{25dB - \overline{SNR}}{s}\right) = Q(-1.58) = 1 - Q(1.58) = 0.943$$

The required SNR will be achieved 94.3% of the time.
